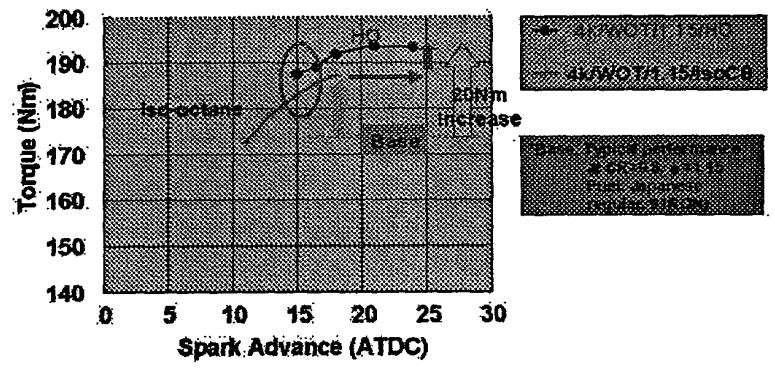


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Figure 1: Torque Performance (4000WOT, CR=13)

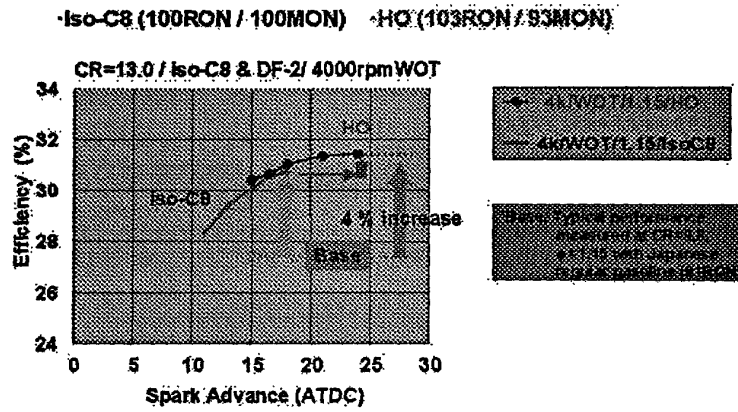
Iso-C8 (100RON / 100MON) Fuel "HO" (103RON / 93MON)



Fuel HO reaches MBT

Torque jump at constant SA → Effect of enhanced burn rate

Figure 2: Efficiency(4000WOT,CR=13)



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Figure 3: Burn Rate and Heat Release Rate

(4000WOT, CR=13,  $\phi=1.15$ , SA=16.5)

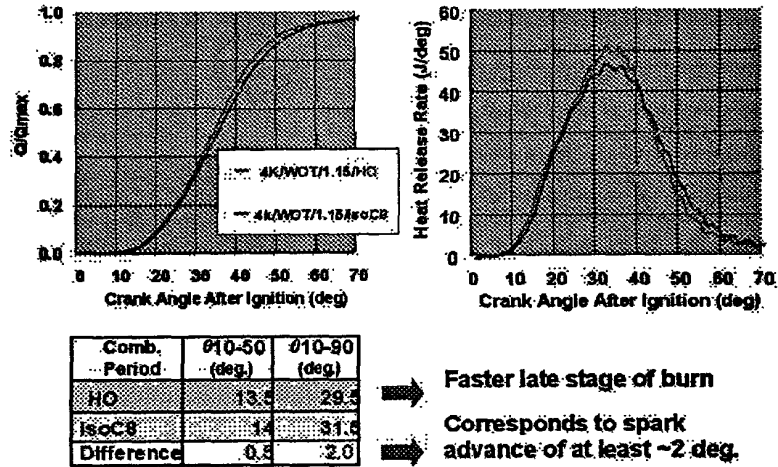


FIGURE 4

1200 rpm, 12mm<sup>3</sup>/st: Inj. Timing Dependence - Torque -  
Spark Timing: 23 deg BTDC

◆ LFG-2B/e13/ $\phi 0.52$   
 ■ DF-1813/ $\phi 0.52$   
 ○ LFG-2B/e9.8/ $\phi 0.52$ /TMC Data

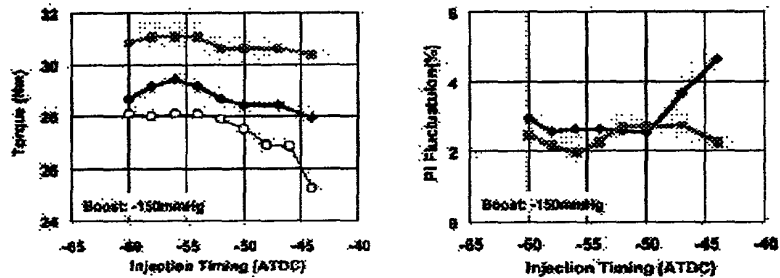


FIGURE 5

1200 rpm, 12mm3/st: Inj. Timing Dependence - Emissions -

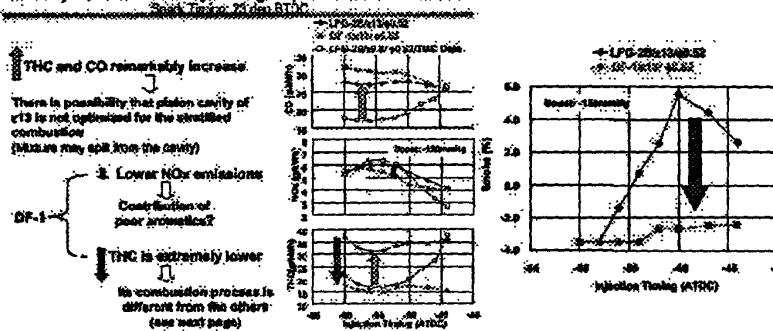
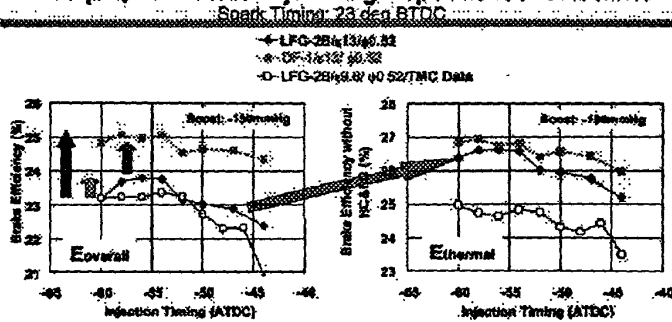


FIGURE 6

1200rpm, 12mm3/st: Inj. Timing Dependence - Efficiencies -



Efficiency: 23.3 => 23.8 ~1.5% UP

LFG-2B => DF-1 ~5.5% UP

Total ~7% UP

Note: Credit from the base (23.3) is expected value because the base data were measured at TMC bench with another engine.

The brake efficiency of #13 series is deteriorated by its higher THC and CO emissions.

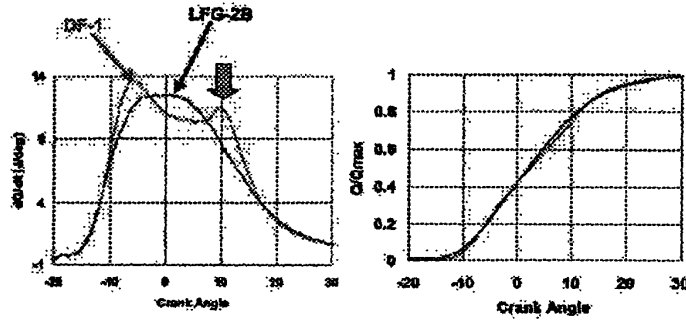
Combination of SICI and low RON aromatics poor fuel is effective for high compression D4.

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FIGURE 7

1200 rpm, 12mm<sup>3</sup>/st: Heat release patterns

Spark Timing: 23 deg BTDC, Inj. Timing: 54 deg BTDC



In the case of DF-1 with  $\phi 13$ , SIC (Spark Induced Compression Ignition) is occurred.

FIGURE 8

3000 rpm, 18mm<sup>3</sup>/st: Inj. Timing Dependence - Emissions -

↑ THC and CO remarkably increase  
There is possibility that piston cavity of  $\phi 13$  is not optimized for the stratified combustion

↓ DF-1  
Lower NOx emissions  
Contribution of poor atomization?

↑ NO  
NO of DF-1 is similar to that of LFG-2B at the same spark timing  
SIC does not occur (see next page)

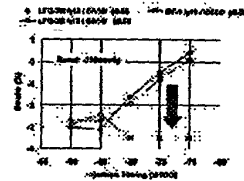
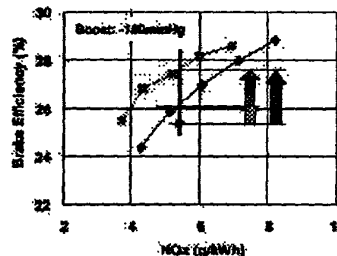


FIGURE 9

3000rpm, 18mm3/st : Credit in Efficiency

Injection Timing: 80 deg BTDC

- ◆ LFG-2B e13 / inj80 / 40.56
- DF-1 e13 / inj80 / 40.56
- LFG-2B e9.8 / inj80 / 40.56 / TMC DATA



Efficiency:

e9.8 ⇒ 13 ~3% UP ↑

LFG-2B ⇒ DF-1 ~5% UP ↑  
(not under equivalent NOx level)

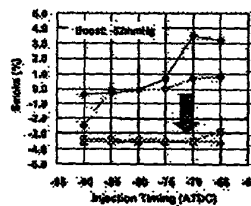
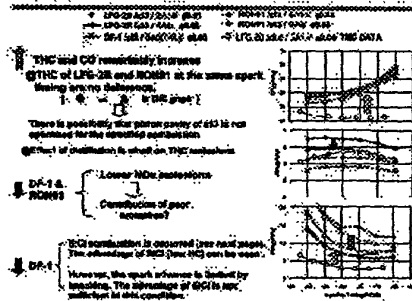
Total ~8% UP ↑

Above credit is not universal

It is not better way to retard  
spark timing in order to reduce  
NOx emissions.

FIGURE 10

2400 rpm, 24mm3/st : Inj. Timing Dependence - Emissions

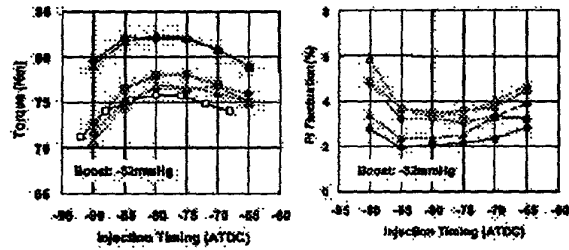


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FIGURE 11

2400 rpm, 24mm<sup>3</sup>/st: Inj. Timing Dependence - Torque -  
Equivalent Boost and  $\Phi$

- LFG-2B /  $\epsilon$ 13 / SA14 /  $\phi$ 0.63      — RON91 /  $\epsilon$ 13 / SA14 /  $\phi$ 0.63  
— LFG-2B /  $\epsilon$ 13 / SA9 /  $\phi$ 0.63      — RON91 /  $\epsilon$ 13 / SA9 /  $\phi$ 0.63  
— DF-1 /  $\epsilon$ 13 / SA9(TKL) /  $\phi$ 0.63      — LFG-2B /  $\epsilon$ 9.8 / SA14 /  $\phi$ 0.64 / TMC DATA

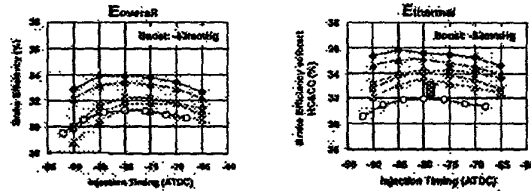


$\epsilon$ 13 series shows higher torque.

FIGURE 12

2400rpm, 24mm<sup>3</sup>/st: Inj. Timing Dependence - Efficiencies -

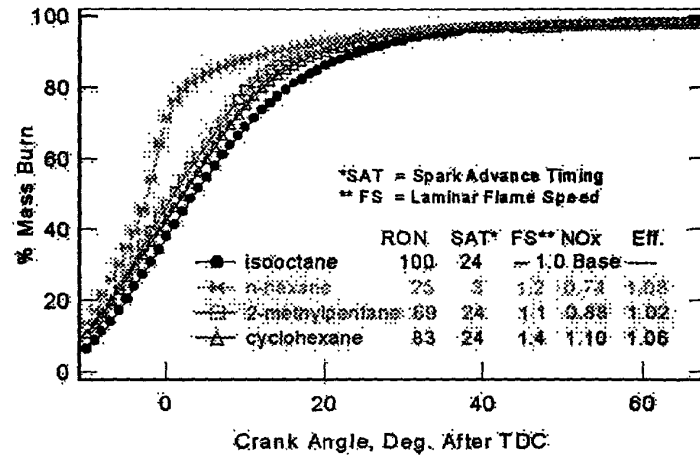
- LFG-2B /  $\epsilon$ 13 / SA14 /  $\phi$ 0.63      — RON91 /  $\epsilon$ 13 / SA14 /  $\phi$ 0.63  
— LFG-2B /  $\epsilon$ 13 / SA9 /  $\phi$ 0.63      — RON91 /  $\epsilon$ 13 / SA9 /  $\phi$ 0.63  
— DF-1 /  $\epsilon$ 13 / SA9(TKL) /  $\phi$ 0.63      — LFG-2B /  $\epsilon$ 9.8 / SA14 /  $\phi$ 0.64 / TMC DATA



Credit in efficiency will be discussed on later page.

The brake efficiency of  $\epsilon$ 13 series is deteriorated by its higher THC and CO emissions

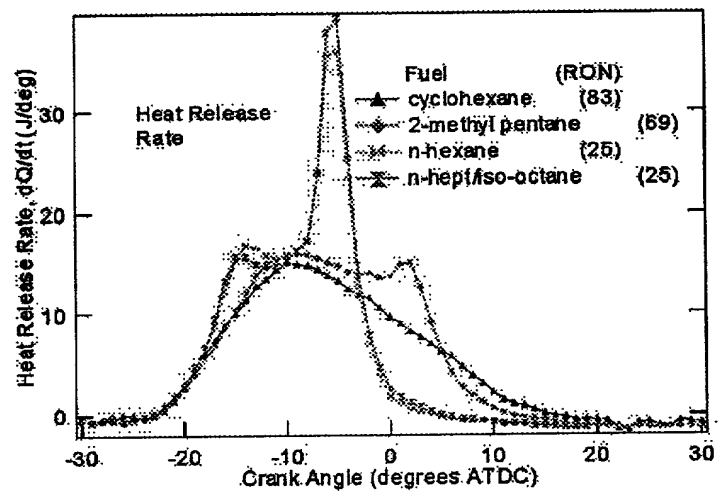
FIGURE 13



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FIGURE 14



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